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Original Research Article

In Situ Catalytic Conversion of Glycerol to Triacetin under Microwave Irradiation with Commercial Palladium on Activated Carbon Catalyst

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ABSTRACT

The depletion of non-renewable fossil fuels has increased the importance of carbon-neutral resources like biofuel and biodiesel. Biodiesel is a better fuel option than petrodiesel due to its excellent lubricity, non-toxic nature, and lack of sulphur. However, the excess production of glycerol is a challenge for biodiesel usage. This study investigates using an acetylation process with palladium on the activated carbon catalyst to convert glycerol into triacetin, a potential fuel additive for biodiesel blends. The study optimises the reaction parameters using response surface methodology to achieve high selectivity for triacetin. The study determined that the optimised parameters for achieving 96.64% glycerol conversion and 0.231% triacetin selectivity are 110 °C, a 1:10 glycerol-acetic acid mole ratio, and 0.718 wt% catalyst loading. Analysis of variance revealed that the reaction temperature significantly impacts glycerol conversion, while the glycerol-acetic acid mole ratio affects the selectivity of triacetin.

KEYWORDS

Glycerol, Activated carbon, Acetylation, Triacetin, Microwave-assisted reaction.

INTRODUCTION

The growth of the biodiesel industry has been increasing rapidly in recent years. Approximately 85 million barrels per day (Mb/d) or 3900 million metric tonnes of oil equivalent (Mtoe) were produced globally in 2010 [1]. The experts predict that future oil production will be around 300 Mb/d by 2100 [2]. Whereas biodiesel production in Malaysia has increased at an average annual rate of 36.41% from zero barrels per day to 29.12 thousand barrels per day between 2000 and 2019, owing to increased demand for local usage and exports [3].

Despite the accelerated progress in the formulation and production of biodiesel, numerous challenges are evolving, and these must be tackled competently. One of the main challenges is

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the unavoidable low-value generation of glycerol (glycerine/1,2,3-propanetriol) as a byproduct of biodiesel from the transesterification process [4]. For every biodiesel production, 10 wt% of glycerol is generated based on stoichiometric reaction balance [5]. Glycerol's global market, estimated to be 2.8 million metric tonnes in 2020, is expected to increase to 4 million metric tonnes in 2027 [6]. Between 2015 and 2019, the value of Malaysian glycerol increased by 1%, while the quantity increased by 3% annually [7]. This excessive glycerol must be converted into value-added chemicals [8], preferably into high-value-added products such as chemicals, oxygenated fuel additives, solvents, and polyesters. Glycerol can produce esters of glycerol such as monoacetin (MAG), diacetin (DAG), and triacetin (TAG) via acetylation with acetic anhydride, ethyl acetate, and acetic acid in the presence of appropriate catalysts [9]. Acetylation of glycerol to produce acetins garnered wide interest from researchers owing to its various applications for the end products, such as a solvent for dyes, plasticisers, etc.

Furthermore, acetins demonstrate exceptional capabilities as fuel additives to decrease carbon monoxide emissions, particulate matter, unburned hydrocarbon emissions, and unregulated aldehydes. They have great potential for enhancing cold flow properties and reducing viscosity when introduced into formulations of diesel and biodiesel [10]. They can also be used as plasticisers of cellulosic polymers and copolymers, antiknock additives for gasoline, and in manufacturing explosives and biodegradable polyesters [8]. Moreover, they are widely utilised as food additives, solvents in leather tanning industries, and the manufacture of cigarette filters [11].

Conventional approaches for the industrial manufacture of triacetin typically require a longer time of reaction and operate at high temperatures. Hence, applying catalysts is recommended to attain a less energy-intensive and lower-temperature process [12]. Therefore, this research focuses on transforming glycerol into high-value products through acetylation to produce triacetin as an economically feasible alternative. Acetylation is the direct esterification between glycerol and acetic acid or acetic anhydride in the presence of appropriate acid catalysts [5]. Over numerous types of catalysts, acetic anhydride as the acetylating agent optimises the reaction with 100% glycerol conversion and more than 90% triacetin selectivity in a shorter reaction time. Nonetheless, this approach is unsuitable because acetic anhydride is more expensive than acetic acid; the reaction is extremely exothermic and risks human health [4]. While some investigators have shown reduced selectivity with acetic acid, few have reported increased triacetin selectivity when using excessive acetic acid to address this constraint [11].

Recently, numerous catalysts have been synthesised and investigated for the acetylation of glycerol with acetic acid. Homogeneous catalysts such as sulphuric acid (H₂SO₄), hydrochloric acid (HCl), or phosphoric acid (H₃PO₄) were used for the acetylation of glycerol. Homogeneous catalysts have a few key drawbacks. Firstly, it is challenging to separate these catalysts effectively, often necessitating the use of neutralisation agents. Secondly, they can cause corrosion problems for the equipment involved. Lastly, using homogeneous catalysts produces significant hazardous waste [13].

Moreover, using homogeneous catalysts is frequently related to insufficient reusability, environmental threats, and reduced purity of the main product [9]. The workaround solution involves using heterogeneous catalysts, which provide multiple benefits, including improved selectivity for desired products, lower toxicity, easy separation, and reusability, unlike homogeneous catalysts [14]. Hence, various studies focused on the development of different types of heterogeneous catalysts such as zeolites [15], heteropoly acids [16], Amberlyst 15 [17], cobalt oxide on tin oxide [18], and ruthenium/copper nanoparticles in mesoporous silica derived from rice husk ash [19] for the esterification of glycerol with acetic acid. However, the selectivity of triacetin is limited for several reasons. These include the decreasing acidity of the catalysts, the successive acetylation of hydroxyl groups, restricted access to acidic sites, the presence of water, and narrow pores. [20]. These gaps allow the researchers to implement different types of solid acid catalysts to substitute for the existing catalyst.

Using carbon-based catalysts for glycerol acetylation shows great promise, as carbon is stable in both acidic and basic environments. This stability makes carbon an attractive choice for glycerol acetylation. Okoye *et al.* have performed glycerol acetylation using the synthesised glycerol-based carbon catalyst [21]. This acetylation reaction converted 99% of the glycerol and produced 88% DAG and TAG. Furthermore, using metal support on activated carbon improves the catalytic activity and selectivity of the targeted compound [22]. Moreover, the doped metal on activated carbon can further maximise its surface area, which can enhance the activity of the catalysts during the esterification reactions [23].

Because of its structural similarity to graphite, AC can be functionalised with groups such as SO₃H, Ph-SO₃H, and so on, just like graphite, fullerenes, nanotubes, or graphene [24]. Researchers used this feature to create sulphonated-active carbons (ACs) with -SO₃H groups. Sulphonated activated carbons are highly researched catalysts anticipated to replace concentrated H_2SO_4 in industries. When utilised as solid acids, they have demonstrated the ability to catalyse various reactions, including cellulose hydrolysis, esterification, nitration, and transesterification [25].

Palladium (Pd) is one of the noble metals that can be active under both acidic and alkaline conditions [26]. Besides, palladium on activated carbon (Pd/AC) catalyst is one of the most widely utilised commercial catalysts in the catalytic process due to its higher catalytic activity and selectivity. Therefore, in this study, Pd/AC was investigated as a solid acid catalyst for glycerol acetylation.

Microwave-assisted heating is an advanced technique in organic reactions that offers shorter reaction times. In contrast, conventional heating methods using a coil or jacket recirculation do not evenly distribute heat throughout the system. In this context, the reaction medium takes longer to reach the desired temperature and often experiences uneven heat distribution due to conduction and convection in conventional heating methods. However, microwave radiation interacts directly with the system without interfering with the molecules in the reaction mixture, eliminating these issues [27].

Microwave irradiation is a process that delivers evenly distributed heating to a reaction medium [28]. Furthermore, microwave-assisted reaction is an easy, clean, and effective method compared to conventional heating [15]. Considering the previously reported findings in the literature, limited research has been done using microwaves in glycerol acetylation using Pd/AC. With the potential of the Pd/AC catalyst as an active catalyst and the ability of microwave irradiation to shorten the reaction time, this research can bridge the gap in the acetylation of the glycerol process. Hence, this underlines the novelty of the present work.

MATERIALS AND METHODS

Acetic acid (purity > 99.85%), glycerol (purity > 99.9%), and palladium on activated carbon (5 wt% Pd) were obtained from Sigma Aldrich Company and utilised without further purification. Triacetin standard (>99.0%) was purchased from Sigma Aldrich (Germany).

Characterisation of palladium on activated carbon

The surface morphology, textural properties, and elemental compositions of the Pd/AC catalyst were studied using Field Emission Scanning Electron microscopy coupled with Energy-Dispersive Spectroscopy (FESEM-EDS; ZEISS SUPRA 35VP) [21].

The thermal stability of Pd/C was analysed using a thermal gravimetric analyser (TGA; Mettler Toledo 851e, Switzerland) at a temperature range of 50 to 600 °C. The heating rate was 10 °C/min in a continuous nitrogen gas flow at 50 mL/min [4].

X-ray diffraction (XRD) patterns of Pd/AC were analysed on a Bruker JDX 8030 phaser using Copper K α radiation ($\lambda = 0.15406$ nm) with a 2 θ range of 2–80° with a step size of 0.02° [29].

NH₃-temperature-programmed desorption (NH₃-TPD) was used to determine the surface acid site density and acid strength of Pd/AC (Micromeritics Autochem II 2920 chemisorption analyser).

The catalyst was evacuated with helium at a rate of 20 mL/min from the surrounding temperature to 150 °C for 1 hour, then cooled to 40 °C, and 15% NH_3 gas was absorbed by the Pd/AC catalyst for 1 hour at a rate of 20 mL/min. [14].

Using a Bruker Alpha spectrometer and the attenuated total reflection (ATR) method, a Fourier transform infrared spectrometer (FTIR) was utilised to analyse the surface and functional groups over a wavenumber range of 400 to 4000 cm⁻¹ [21].

Experimental setup

The acetylation of glycerol reactions using acetic acid was conducted in a 250 mL threenecked round bottom flask in a microwave reactor setup, as shown in **Figure 1**. Chill water continuously flows through the condenser coil to prevent the evaporation of reactants under atmospheric pressure.

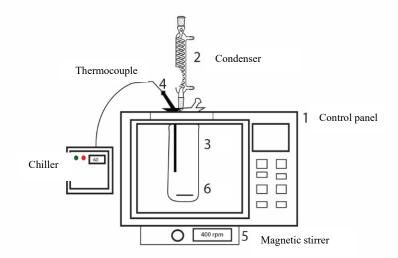


Figure 1. Schematic diagram of experimental equipment [15]

Firstly, a fixed amount of Pd/AC catalyst and glycerol (**Table 1**) were mixed in a 100 mL beaker. The Pd/AC catalyst and glycerol mixture, followed by acetic acid, was transferred to a 250 mL three-necked round-bottom flask. The reaction flask was then placed into the microwave chamber. The reaction was started initially at a low micropower setting. The reaction was run for 90 min and continuously stirred using a magnetic stirrer at 400 rpm. At the end of the reaction, the mixture was cooled to room temperature and filtered to separate the Pd/AC catalyst from the reactant. The mixture of the reactant was then transferred to a sampling bottle and stored for triacetin analysis using gas chromatography with flame ionisation detection (GC-FID) analysis as described and high-performance liquid chromatography (HPLC) for glycerol conversion [9].

Product analysis

The liquid product from acetylation of glycerol was analysed by gas chromatography (GC, Agilent 7820A with autosampler 7683) equipped with a flame ionisation detector (FID) and a capillary column (HP-5, 30 m×0.32 mm, 0.25 μ m). Helium was used as a carrier gas at 25 mL/min. The injector and detector were set at 280 °C and 320 °C, respectively. External calibration for triacetin standard samples was prepared. Samples were prepared by mixing 700 μ L of ethanol (GC grade) with 500 μ L of the product as the internal standard. Firstly, 1 μ L of the sample was injected at 70 °C, then increased up to 270 °C at the rate of 70 °C/min and detained for 2 min, and finally increased to 300 °C at the rate of 20 °C/min. Triacetin was detected based on its retention times using the GC-FID, which was pre-calibrated and determined by relative peak areas [9]. The glycerol conversion was determined by HPLC using an Agilent Hi-Plex H column (7.7 × 300 mm,

 $8 \ \mu\text{m}$) at 65 °C under an oven with mobile phase 0.005 M sulphuric acid and a flow rate of 0.6 mL/min using a refractive index detector. The external calibration curve was prepared for glycerol conversion [30].

Experimental design for optimisation of the acetylation of glycerol

Each Central Composite Design (CCD, Design-Expert[®] version 10 software) was used to design the independent factors that affect the acetylation of glycerol. **Table 1** shows the list of the variables and their ranges used for this analysis. Fifteen experimental runs were constructed, with one run anticipated to authenticate the effectiveness of the measured parameters on the results. The three independent factors include temperature (80-110 °C), acetic acid: glycerol mole ratios (5-10), and Pd/AC catalyst loadings (0.5-2.5 wt%) using three levels for each factor. Two dependent variables were assessed after each experimental run.

Table 1. Design parameters for acetylation of glycerol using a Pd/AC catalyst

Name	Unit	Low	High	-alpha	+alpha
Temperature	°C	80	110	73.7868	116.213
Molar ratio		5	10	3.96447	11.0355
Catalyst loading	%	0.5	2.5	0.0857864	2.91421

The glycerol conversion and the triacetin selectivity were determined using eq. (1) and eq. (2):

$$Glycerol \ conversion, GC \ [\%] = \frac{Moles \ of \ converted \ glycerol}{Moles \ of \ initial \ glycerol} \times \ 100$$
(1)

$$Triacetin \ selectivity, TS \ [\%] = \frac{Moles \ of \ triacetin \ produced}{Mole \ of \ glycerol \ reacted} \times \ 100$$
(2)

Statistical analysis

The importance of the independent factors and the correlation between these parameters were analysed using ANOVA (p < 0.05). The role of the independent factors in the acetylation of glycerol as a function of the quadratic model was determined by the adjusted coefficient of determination (R^2 Adj.). Moreover, the relationship between the independent factors and their effect on the acetylation of glycerol was represented in three-dimensional (3D) graphical plots of response surface methodology (RSM).

RSM is crucial in examining the relationships between multiple variables and optimising complex processes. By utilising RSM, the response of a system to various experimental factors can be effectively analysed, and mathematical models can be derived to represent the relationship between these factors and the response variable. It enables the identification of optimal process conditions and the prediction of responses within a defined experimental space. Overall, statistical analysis using RSM enhances the understanding of complex systems and aids in optimising processes by providing valuable insights into the interactions and effects of multiple variables.

RESULTS AND DISCUSSION

The external morphology of the Pd/AC is presented in **Figure 2**. The results revealed that the Pd/AC catalyst particles had non-uniform shapes. The EDX results of the Pd/AC composition are shown in **Table 2**. The EDX spectra confirmed the presence of the chemical constituents for Pd/AC as, in weight per cent, Pd = 1.96%, C = 97.04%, Si = 0.67%, and Cl = 0.34% and atomic per cent, Pd = 0.23%, C = 99.36%, Si = 0.29%, and Cl = 0.12%. The diffraction peaks' strong intensity and narrow width for Pd/AC indicate highly crystalline particles. However, the presence of other elements, such as Si and Cl, in the EDX spectrum

shows the occurrence of impurities, as the Pd/AC catalyst used in this investigation was a commercially available catalyst.

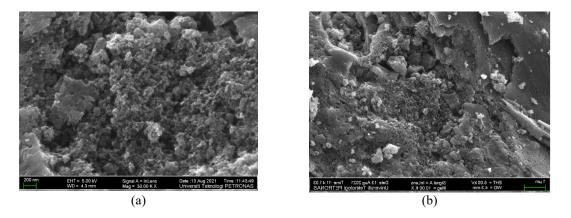


Figure 2. FESEM images of Pd/AC at 200 nm (a) and 1 μ m magnification (b)

Component	Weight [%]	Atomic [%]
Carbon	97.03	99.36
Palladium	1.96	0.23
Silicon	0.67	0.29
Chloride	0.34	0.12

Table 2. Elemental composition of the catalysts

The thermal decomposition of the Pd/AC catalyst was investigated by TGA, as shown in **Figure 3**. The catalyst exhibited two major weight losses. The first weight loss was detected in the 80–90 °C range, and the second between 390–500 °C. The first weight loss below 100 °C is attributed to the loss of moisture or water molecules and the disintegration of small-molecule end-groups such as C–N, C–H, and C=O. The second weight loss is attributed to decomposing functional groups in Pd/AC. It designates the high stability of the Pd/AC catalyst and could be utilised at a temperature below 250 °C [20].

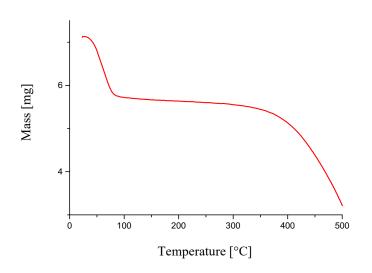


Figure 3. TGA profile of Pd/AC

XRD was used to analyse the composition and phase purity of the Pd/AC. XRD patterns of Pd/AC are presented in **Figure 4**, showing diffraction peaks with 20 values at 21.24°, 26.95°, 34.42°, 40.49°, 47.04°, 50.49°, and 68.52°. The broad band observed between 20–30° is characteristic of amorphous materials, which confirms that Pd/AC has a low degree of crystallinity with hexagonal graphite [22]. These are associated with sp²-bonding carbon deficient in periodicity in the C-axis. The presence of Pd does not alter the structure of the AC and will not affect its resistance to high-temperature reactions [22]. The diffraction peaks at 26.95° and 47.04° are attributed to the carbon structure of activated carbon. The main peak at 40.49° suggested that a crystal phase was formed [31]. The presence of Pd in the samples caused weaker peaks of activated carbon. Besides, it is well acknowledged that the X-ray patterns of metal species are not detected as metals are vastly disseminated on the support [29].

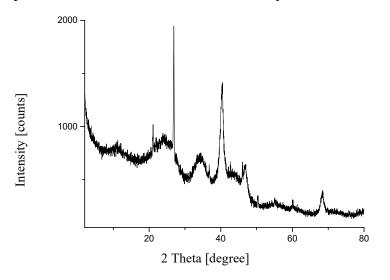


Figure 4. XRD patterns of Pd/AC

NH₃-TPD results for the Pd/AC are shown in **Figure 5**. Two notable desorption peaks occur between 760 and 740 °C and around 840 °C, which are strong medium acid strength regions. The first desorption peak is ascribed to functional groups such as -COOH and -OH. The second peak is linked with the decomposition of carbon materials, including desorption of the -CO surface with phenolic and carbonyl functional groups. The Pd/AC also showed high acid site density, offering a sufficient anchoring site for the reaction of the acetylation of glycerol [20].

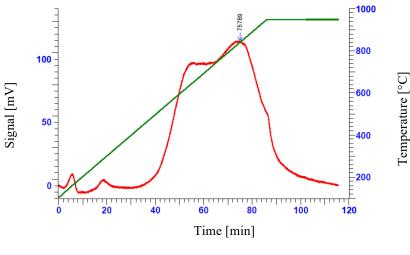


Figure 5. NH₃-TPD of Pd/AC

The FTIR spectrum of Pd/AC is depicted in **Figure 6**. The peaks were detected at 1581.95 cm⁻¹ and 1224 cm⁻¹, representing the stretching vibrations of C=O and C=C and the bending vibration of the C–O–C groups, respectively [32]. C=C bonds in activated carbons are undoubtedly observed within the wavenumber range of 1700 cm⁻¹ to 1600 cm⁻¹ [33]. The peak at 1091.79 cm⁻¹ is related to C–O stretching vibrations, while the peak at 2345.99 cm⁻¹ is associated with C–H stretching vibrations. The intense band at 3422 cm⁻¹ is due to the stretching vibrations of –OH groups. Similarly, Ya'Aini *et al.* [33] observed the peaks of Pd/AC around 3648 cm⁻¹ and 1200 cm⁻¹, typically due to the presence of hydroxyl and C–O groups, respectively. Moreover, they also detected a band at 1550 cm⁻¹, possibly due to the stretching vibration C=O in the carboxyl, aldehyde, and ketone groups.

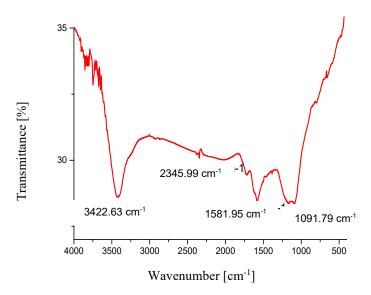


Figure 6. FTIR spectrum of Pd/AC

Optimisation of the acetylation of glycerol

The optimisation of parameters for the glycerol acetylation using Pd/AC as the catalyst was conducted using Design-Expert software Version 12.

	Factor 1	Factor 2	Factor 3	Response 1	Response 2
Run	A:	B: Molar	C: Catalyst	Triacetin	Glycerol
Kull	Temperature	ratio	loading	selectivity	conversion
	[°C]	[-]	[%]	[%]	[%]
1	95	7.5	1.5	0.028	96.53
2	110	10	0.5	0.220	96.65
3	110	5	2.5	0.193	96.53
4	80	5	0.5	0.000	96.43
5	95	11.04	1.5	0.021	96.62
6	80	10	2.5	0.000	96.54
7	95	3.96	1.5	0.000	96.44
8	95	7.5	1.5	0.043	96.54
9	95	7.5	1.5	0.040	96.54
10	95	7.5	1.5	0.024	96.53
11	73.79	7.5	1.5	0.000	96.50
12	95	7.5	2.91	0.019	96.53
13	95	7.5	0.09	0.022	96.52
14	95	7.5	1.5	0.033	96.53
15	116.21	7.5	1.5	0.463	96.54

Table 3. Experimental design with triacetin selectivity and glycerol conversion

The maximum value for the glycerol conversion of 96.65% was recorded at Run 2. In contrast, the maximum triacetin selectivity was 0.463% at Run 15 (**Table 3**). Glycerol acetylation is an acid-catalysed reaction that needs acid sites with adequate strength [32]. The synthesis of triacetin through acetylation includes the transfer of a proton from the Pd/AC catalyst, which activates the carbonyl group of acetic acid and results in an elevated positive charge. The oxygen molecule of glycerol will attack the protonated acetic acid, which leads to the formation of monoacetin with the loss of one water molecule. The formed monoacetin was then further broken down into diacetin and triacetin in a sequence of reactions [9].

Analysis of variance

According to the response surface methodology model fit, the quadratic model had the best fit in defining the impacts of parameters on triacetin selectivity. **Table 4** shows the summary of the analysis of variance for the regression model for triacetin selectivity. The Model F-value of 286.22 implies the model is significant. In this case, temperature (A), molar ratio (B), catalyst loading (C), enhanced temperature parameter (A^2), enhanced molar ratio (B^2), and enhanced catalyst loading (C^2) are significant model terms as the probability (p) values are less than 0.0500. Values greater than 0.1000 indicate the model terms are not significant. The Lack of Fit F-value of 2.98 implies the Lack of Fit is non-significant relative to the pure error. There is a 15.93% chance that a Lack of Fit F-value this large could occur due to noise. A nonsignificant lack of fit is good, which means it suits the model. Besides, the model's high R² value (0.9981) shows that the data is evaluated accurately. The Predicted R² of 0.9089 is in reasonable agreement with the Adjusted R² of 0.9946, where the difference is less than 0.2.

Source	Sum of Squares	df	Mean Square	F-value	p-value	
Model	0.2252	9	0.0250	286.22	< 0.0001	significant
		9				C
A – Temperature	0.1071	I	0.1071	1225.81	< 0.0001	significant
B – Molar ratio	0.0002	1	0.0002	2.56	0.1703	not significant
<i>C</i> – Catalyst loading	2.307E-06	1	2.307E-06	0.0264	0.8773	not significant
AB	0.0001	1	0.0001	0.8831	0.3905	not significant
AC	5.209E-07	1	5.209E-07	0.0060	0.9414	not significant
BC	0.0073	1	0.0073	83.48	0.0003	significant
A^2	0.0711	1	0.0711	813.71	< 0.0001	significant
B^2	0.0016	1	0.0016	18.35	0.0078	significant
C^2	0.0007	1	0.0007	7.87	0.0377	significant
Residual	0.0004	5	0.0001			
Lack of Fit	0.0002	1	0.0002	2.98	0.1593	not significant
Pure Error	0.0003	4	0.0001			
Cor. Total	0.2255	14				

Table 4. Analysis of variance for the regression model for triacetin selectivity

To assess the results, regression analysis was performed on the data in Table 4 using the quadratic equation:

Triacetin selectivity = 3.07203 - 0.071454A - 0.014382B - 0.156842C + (3) $0.000166AB + 0.000034AC + 0.024157BC + 0.000427A^2 - 0.002306B^2 - 0.009443C^2$

Figure 7 shows the predicted vs. actual values for the triacetin selectivity. Almost all the points of the actual values lie on the formulated predicted line. The lack of fit test was non-significant, indicating that the model can accurately predict triacetin selectivity within the specified range of factors.

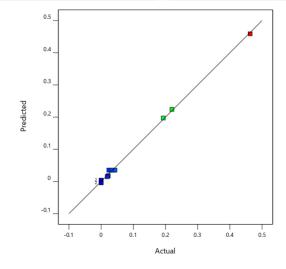


Figure 7. Predicted vs. actual values for the triacetin selectivity

Based on the p-value in **Table 4**, the significant model terms are temperature (*A*), combination molar ratio and catalyst loading (*BC*), enhanced temperature (A^2), enhanced molar ratio (B^2), and enhanced catalyst loading² (C^2). The higher temperature will impact the selectivity of triacetin [34]. It has also been proven based on the graphs in Figures 8a and 8b; as can be seen, the higher the reaction temperature, the higher the triacetin selectivity.

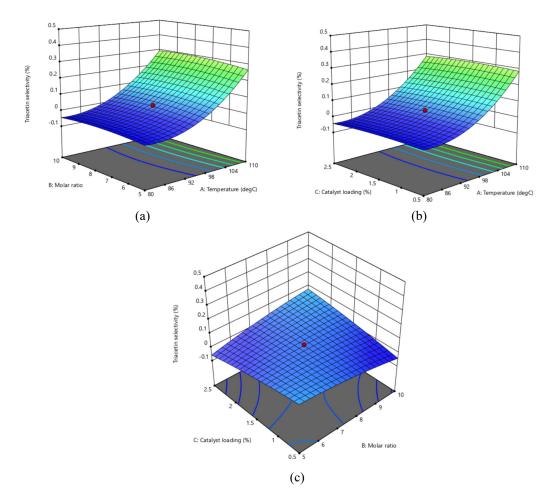


Figure 8. Impacts on triacetin selectivity: effect of temperature [°C] and molar ratio (a); effect of catalyst loading [%] and temperature [°C] (b); effect of catalyst loading [%] and molar ratio on triacetin selectivity (c)

The quadratic model was shown to be the best-fitted model for conceptualising the impacts of the parameters for the second response, which is the conversion of glycerol. **Table 5** displays a summary of the analysis of variance for the glycerol conversion regression model. The model is significant, as shown by the Model F-value of 411.92; it might occur due to noise only 0.01% of the time. Important model terms with p-values less than 0.0500 include temperature (*A*), the molar ratio (*B*), and the molar ratio & catalyst loading (*BC*). The lack of fit was not significant compared to the pure error (F-value of 0.0569). A significant Lack of Fit F-value has an 82.32% chance of being caused by noise, indicating a solid model. The discrepancy between the Predicted R² of 0.9960 and the Adjusted R² of 0.9758 is less than 0.2, i.e., in fair agreement.

Source	Sum of Squares	df	Mean Square	F-value	p-value	
Model	0.0430	9	0.0048	411.92	< 0.0001	significant
A - Temperature	0.0010	1	0.0010	82.67	0.0003	significant
B – Molar ratio	0.0148	1	0.0148	1280.21	< 0.0001	significant
<i>C</i> – Catalyst loading	0.0012	1	0.0012	104.28	0.0002	significant
AB	0.0006	1	0.0006	48.22	0.0010	significant
AC	0.0000	1	0.0000	1.64	0.2570	not significant
BC	0.0028	1	0.0028	245.61	< 0.0001	significant
A^2	0.0003	1	0.0003	27.88	0.0032	significant
B^2	0.0000	1	0.0000	1.65	0.2551	_
C^2	0.0009	1	0.0009	75.74	0.0003	significant
Residual	0.0001	5	0.0000			
Lack of Fit	8.133E-07	1	8.133E-07	0.0569	0.8232	not significant
Pure Error	0.0001	4	0.0000			-
Cor. Total	0.0430	14				

Table 5. Analysis of variance for the regression model for glycerol conversion

Eq. (4) depicts the final empirical models of the proposed quadratic model in terms of the three real variable components. The negative signs in front of the phrases imply antagonistic effects, whereas the positive marks indicate synergistic effects [35].

Glycerol conversion = 95.57119 + 0.009534A + 0.093139B + 0.044304C - 0.000446AB + (4) $0.000205AC - 0.015093BC - 0.000029A^2 - 0.000252B^2 + 0.010669C^2$ (4)

Figure 9 shows that the points were scattered near the predicted line. The R-squared value is 0.9862, and the lack of fit test was also found to be non-significant, indicating that the model can accurately predict glycerol conversion within the specified range of factors.

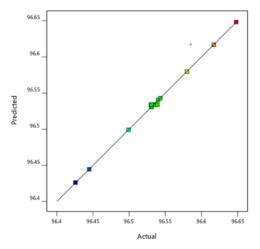


Figure 9. Predicted vs. actual values for the glycerol conversion

By referring to the p-value in **Table 5**, the significant model terms are temperature (*A*), the molar ratio (*B*), catalyst loading (*C*), temperature & catalyst loading (*AC*), molar ratio & catalyst loading (*BC*), squared temperature (A^2), and squared catalyst loading (C^2). The higher temperature and molar ratio influenced the glycerol conversion. Besides, this has also been proven based on the graphs in **Figures 10a** and **Figures 10b**; as can be seen, the higher the reaction temperature, the higher the percentage of triacetin selectivity.

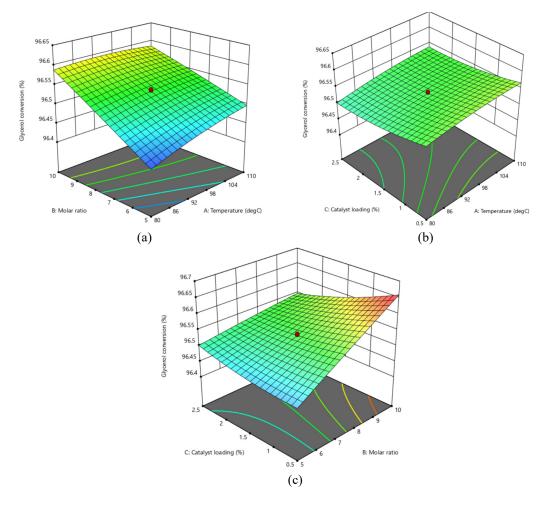


Figure 10. Impacts on glycerol conversion: effect of temperature [°C] and molar ratio (a); effect of catalyst loading [%] and temperature [°C] (b); effect of catalyst loading [%] and molar ratio (c)

Effect of reaction temperatures

The effect of reaction temperature (80°C to 110°C) on glycerol conversion and product selectivity was investigated at a 90 min reaction time. The interaction between reactants and catalysts increases as the temperature increases. Moreover, an increase in temperature reduces the viscosity of glycerol and enhances its solubility [36]. It can also enhance the diffusion of reactants and products in and out of the active sites. It is also known that high triacetin selectivity and glycerol conversion are achieved at high temperatures as it is an endothermic process [37].

The triacetin selectivity increased drastically as the temperature increased at the expense of monoacetin and diacetin. It shows the necessity of temperature to convert monoacetin and diacetin to triacetin efficiently. Triacetin and glycerol conversion selectivity were best at 116 °C and 110 °C, respectively. Nevertheless, further increments in temperature above 110 °C lead to decreased selectivities due to the reduced accessibility of acetic acid, which causes it to evaporate at a higher rate [9]. Moreover, collisions between atoms increase at higher reaction temperatures [36].

Effect of reactant molar ratio

Acetylation of glycerol can be enhanced by instigating one of the reactants in excess. Three moles of acetic acid and one mole of glycerol are needed to produce one mole of triacetin. The conversion of glycerol was increased by increasing the glycerol/acetic acid molar ratio up to 1:10. As glycerol acetylation is a reversible reaction, the surplus of acetic acid in the reaction mixture improves the reaction towards the conversion of glycerol but not the triacetin selectivity. The optimum conversion of 96.64% was attained at the glycerol/acetic acid ratio of 1:10. Additionally, excessive usage of acetic acid in the acetylation of glycerol reduces the time required to accomplish equilibrium. It offers more acetylation agents that produce triacetin with further acetylation. Hence, it can be deduced that an increase in the molar ratio between acetic acid and glycerol will increase glycerol conversion [36]. Though it must be noted that a further increase in molar ratios does not cause any changes in triacetin selectivity or glycerol conversion, more acetic acid molecules would attach to the same active sites at Pd/AC [9].

Effect of catalyst loading

As the Pd/AC loading increases, the selectivity of triacetin and the conversion of glycerol improve due to the availability of more active sites on Pd/AC [38]. Yet, the reaction efficiency declines if the Pd/AC loading is increased beyond a certain point because the particles start to aggregate, reducing the access of reactants to the Pd/AC catalyst and impeding the transfer rates to active sites within the aggregates. Using a moderate catalyst amount is advisable to achieve high glycerol conversion and selectivity towards triacetin [9].

The role of triacetin in the circular economy

The production of glycerol from biodiesel, using either vegetable oil or animal fat, results in oxygenated additions that are biodegradable, non-toxic, and renewable. Three classes of oxygenated additives can be distinguished: acetins, glycerol ethers, and glycerol formal. These gasoline additives made from the conversion of glycerol could replace traditional petroleumbased additives like ethyl tert-butyl ether and methyl tert-butyl ether. Fuel additives are often used to enhance engine performance and reduce various engine components' corrosion [39].

Moreover, employing triacetin as a fuel additive can lead to significant reductions, such as up to 75% in hydrocarbon (HC) emissions, around 10% in carbon dioxide (CO₂) emissions, 50% in carbon monoxide (CO) emissions, and 28 to 29% in nitrogen oxide (NO) emissions, compared to diesel and non-blended biodiesel [40]. This finding showed another positive outcome in applying blended biodiesel with glycerol-based fuel additives. It can also improve biodiesel's economics by reducing its manufacturing costs, in line with the circular economy and net-zero carbon emission frameworks.

The environment, raw material supply security, competitiveness, innovation, economic growth acceleration, and creation of jobs may all benefit from a more circular economy. Additionally, customers will receive more innovative and long-lasting products, which will enhance their quality of life and help them save money in the long run [41].

CONCLUSIONS

The Pd/AC catalyst enhanced the efficiency of glycerol acetylation under microwave irradiation, responding to the independent factors. The temperature of 110 °C, the glycerol and acetic acid molar ratio of 1:10, and the catalyst load of 0.718 wt% were found to be the best conditions for generating high triacetin selectivity and glycerol conversion after utilising RSM to optimise the reaction parameters. The increase in reaction temperature is one of the parameters that can increase triacetin selectivity.

The biodiesel industry is growing with increasing demand and produces a surplus of glycerol that can be used as a fuel additive. Also, the availability of a suitable and active green catalyst at a low cost will enhance the production of acetins, especially triacetin.

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NOMENCLATURE

Abbreviations

ANOVA	Analysis of variance
CCD	Central composite design
FESEM-EDS	Field emission scanning electron microscopy coupled with energy-dispersive spectroscopy
FTIR	Fourier transform infrared spectrometry
GC	Glycerol conversion
GC-FID	Gas chromatography with flame ionisation detection
HPLC	High-performance liquid chromatography
NH ₃ -TPD	Ammonia-temperature programmed desorption analysis
Pd/AC	Palladium on activated carbon catalyst
RSM	Response surface methodology
TGA	Thermogravimetric analysis
TS	Triacetin selectivity
XRD	X-ray diffraction

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