

# Journal of Sustainable Development of Energy, Water and Environment Systems

http://www.sdewes.org/jsdewes



Year 2025, Volume 14, Issue 1, 1130631

### **Original Research Article**

# Biogas Venting from Household Biogas Technology Use in the Sub-Saharan Africa: Evidence from Rwandan Households as a Case

# James Ntaganda\*1,2, Basílio Z. S. Tamele<sup>1</sup>, Erik O. Ahlgren<sup>1</sup>

<sup>1</sup>Chalmers University of Technology, Department of Space, Earth and Environment, Division of Energy Technology, SE- 41296, Gothenburg, Sweden

Cite as: Ntaganda, J., Tamele, B. l. Z. S., Ahlgren, E. O., Biogas Venting from Household Biogas Technology Use in the Sub-Saharan Africa: Evidence from Rwandan Households as a Case, J.sustain. dev. energy water environ. syst., 14(1), 1130631, 2025, DOI: https://doi.org/10.13044/j.sdewes.d13.0631

#### **ABSTRACT**

Household biogas technology can potentially contribute to the dean cooking transitioning. However, when improperly used, and not well customised to the user's cooking needs and practices, the technology can lead to counterintuitive and detrimental thenomena, e.g. venting. This does not only affect the technology's effective use but also its climate benefits. This work aims to estimate greenhouse gas emissions associated with biogas venting from household biogas technology use and establish its causes. Household biogas utilisation data were collected remotely by using smart biogas meters and validated with conventional analogue pressure gauges. The remotely acquired data were analysed to understand the household biogas utilisation and venting levels from Rwandan households as case for the study. Results showed that the ratio of biogas utilisation to venting was N:1. Biogas lost through venting resulted into average monthly emissions of 33–56 kgCO<sub>2,e</sub> per household. Interactive interviews and field observations indicated that the current household biogas systems are not customised to the local cooking practices and the required leating for cooking specific Rwandan staple meals. This results into underutilisation of the produced biogas, leading to venting, hence greenhouse gas emissions. Custom sing the household biogas systems to local cooking practices and or adjusting cooking practices to be technology designs can increase biogas utilisation, minimise venting and enhance envisaged technology benefits.

### KEYWORDS

Clean cooking, Household biogas, Sub-Saharan Africa, Rwanda, Venting, Greenhouse gas emissions

# INTRODUCTION

Biogas produced from family-sized biodigesters is used as a clean source of energy for household cooking within energy-poor communities [1]. Also, in communities with relatively developed energy systems, the technology has been suggested for manure management [2]. Biogas produced through anaerobic digestion (AD) of biodigestible organic matter is mainly composed of methane (40–75%) and carbon dioxide (15–60%) [3]. Other minor amounts of gases and halogenated hydrocarbons are also produced in the process [4]. Of the produced

-

<sup>\*</sup> Corresponding author

biogas composition, combustible methane (CH<sub>4</sub>) is the targeted component for cooking. In response to the global agenda of meeting the SDG 7, specifically its indicator SDG 7.2.1, household biogas technology has been deployed in big numbers in South and South-East Asia and in sub-Saharan Africa (SSA). It is estimated that China alone has more than 40 million biodigesters installed [5]. Through the Africa Biogas Partnership Programme (ABPP), more than 100 thousand household biogas plants were installed 2009–2021 in 11 SSA countries [3]. The increased installation of the technology for the production and use of biogas at household level is motivated by its benefits, e.g., mitigation of health issues associated with the use of solid biomass and fossil cooking fuels [6], household financial savings as a result of reducing energy expenditures [7], environmental benefits and hence global warming mitigations [8], organic manure for soil fertilisation and soil management [9] and other socio-conomic benefits [10].

However, in order to achieve the forementioned benefits of the technology, biogas production and use requires proper system operations and management [11]. In some situations, feedstock may be pretreated to increase the quality and quantity biogas production [12]. Due to the decentralised nature of household biogas technology (HHBT) systems and the fact that daily operational routines are carried out at the household level by household (HH) family members, these systems are often susceptible to inefficiencies in operation and use. This has led to a substantial number of nonfunctional and or poorly operated HH biogas plants within user communities [13]. Thus, there is a growing concern over the technology's sustainable use and achieving its intended benefits [13]. It has been evidenced that even in experienced technology user communities, only about 60% of the domestic biogas plants are operated efficiently [14]. Biogas leakage is one operation is the which not only affects the fuel resource conversion efficiency but also the technology's climate benefits. Hou et al. [15] show that the annual biogas produced from 8m<sup>3</sup> biodigesters installed in Chinese rural dwellings vary between 47–176 m<sup>3</sup> depending on the region. In the same study, it is shown that 59%–61% of the produced biogas is used, while the rest is considered as biogas leakages to atmosphere [15]. Studies continue to report significant environmental benefits of the technology but also caution that when the technology is not well operated, biogas leakages do affect the intended environmental benefits [16]. Dung et al. Show that there is an unfulfilled potential of HH biogas to mitigate global warming due to the fact that about 40% of biogas is lost through leakages [17]. Nevertheless leakage sources in small-scale household biogas systems are frequently generalised, thus overlooking the social contexts of use and the technological diversity in biodigester designs

Contrary to the small-scale HH biogas use, methane emissions from larger-scale production units have been well studied, documented, classified and tracked according to their sources [18]. At large-scale production level, methane is emitted from flaring, venting, fugitive leakages of through combination of these [18]. Such classification at large-scale use helps in estimating greenhouse gas emissions (GHGEs) and developing their mitigation pathways. As shown in Figure 1, venting is an eminent source of methane emissions from large-scale production plants [18]. However, studies on venting from decentralised small-scale use in households within the technology user communities and its possible detrimental effects are lacking in literature, leading to uncertainty in developing mitigation approaches. Biogas venting levels associated with HHBT use could be potentially worse in communities with new technology adopters, e.g. in SSA communities. This leaves a literature gap, calling for studies on GHGEs caused by venting associated with HH biogas production and use.

While studying the HHBT in the SSA technology user communities, Robinson et al. [19], used qualitative research methods to study the venting phenomenon in what they termed as 'opening the pandora box'. Their qualitative findings show that venting is understudied, and call for empirical research approaches, quantifying GHGEs associated with the venting phenomenon [19]. The lack of empirical studies with quantitative measurement approaches to study the biogas venting leads to a lack of knowledge on the carbon footprint from the small-

scale bioenergy sector. This can potentially hinder the growth of emerging voluntary carbon markets and bonds aimed to promote HH biogas technology use in energy-poor communities. For example, Strubbe et al. [20] have generated insights on net-GHGEs as a result of HH biogas technology in Rwandan households, in the Huye District. They have shown that a 4m³ HH biodigester can satisfy up to 65% of the HH cooking energy demand for a family of six members, leading to annual GHGEs reduction of about 2.4 tCO<sub>2,e</sub> per HH when compared to HHs using wood only as cooking fuel.

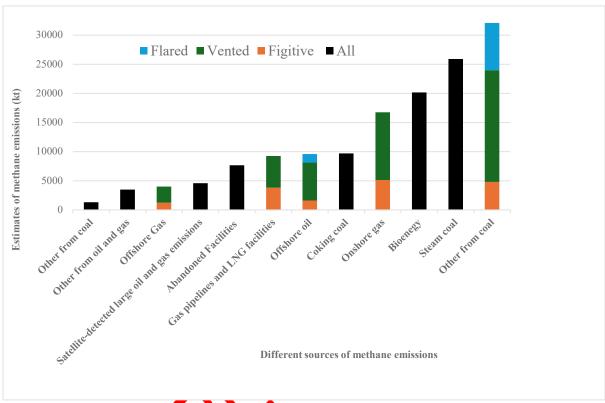


Figure 1. World methane emissions from large-scale energy sources (kt) 2024 [18].

Further, Strubbe et al. [10] show that when the produced digestate is used as a soil fertiliser, the net-GHGEs reduction is enhanced, resulting in an annual reduction of GHGEs of about 2.5 tCO<sub>2,e</sub> per HH. Such results confirm the HH biogas technology benefits, but their estimations are based on a general assumption that the biogas leakage is about 9% of the total produced biogas from a HH biodigester [20]. Such generalised estimations do not clearly distinguish whether leakages through outlets are intentional (venting to avoid biodigester damage) or unintentional due to damages. When the 9% [20] is compared with 40% [17] of biogas losses due leakages, the discrepancy indicates that leakages is context-dependent and leads to a gap worthy of filting, hence contributing to the literature on the HHBT use. The discrepancies in the literature on HH biogas leakage and the lack of literature on biogas venting from HH biogas use formed the basis of our study. Thus, this paper aims to study the venting phenomenon associated with HH biogas use, and attempts to answers three research questions (RQs):

 $RQ_1$ : What are the biogas venting levels associated with HH biogas technology use?  $RQ_2$ : To what extent does venting from HH biogas technology contribute to GHGEs?  $RQ_3$ : What are the causes of venting from HH biogas plants in rural SSA contexts?

To answer the three RQs, Rwandan HHs are used as a case for the study. The novelty and contribution of this paper can be seen in four aspects: Venting is distinguished from generalised biogas leakage in the context of HHBT use. The use of modern smart biogas metres (SBMs)

together with conventional analogue pressure gauges (APGs) provide reliable data for analysing the venting phenomenon not provided by the existing literature. A community-embedded research approach provided a good opportunity to establish and explain the potential causes of biogas venting from within technology-user communities. Based on established causes of venting, we propose potential mitigation approaches which call for further studies.

### **METHODS AND MATERIALS**

In this section, methods and materials are first presented in a general context and then applied to Rwanda as a case used for the study. Methods and materials used are presented in a manner that attempts to answers the three RQs step by step from RQ<sub>1</sub> to RQ<sub>3</sub>.

### Methods

Quantifying biogas venting. The process is guided by recommended principles of HH biodigester designs. There is a maximum (threshold) biogas pressure a biogas holder can handle for a safe HHBT operation, beyond which the produced biogas should be intentionally released (vented) [21]. In Figure 2, the upward arrows illustrate that blogas is continuously collected in the biogas holder while being produced whenever the absolute static biogas pressure (SBP) is still less than the venting threshold. When the produced biogas is underutilised and SBP surpasses the designed threshold value, the pressure can be greater than the compression forces of the biodigester and gas holder, causing potential cracks, hence biodigester damages and biogas leakage. To avoid this, a maximum allowable SBP for a safe operation is determined based on biodigester technology to be installed. When the biogas pressure is just above the threshold value, and no auxiliary storage available, the produced biogas must be intentionally released (vented) to avoid the cracking of the biodigester, allowing the produced biogas to flow through a designed outlet. The venting phenomenon is illustrated in Figure 3. The bidirectional arrows indicate that during venting events, any produced biogas that causes the SBP to just exceed the venting SBP must be released through designated outlet (s). The intentional release can be done by triggering (through designated biogas valves) or by biodigester design, e.g. differential height, a design mechanism used for fixed dome HH biodigesters. Based on this safety design principle, the vented biogas (m<sup>3</sup>) can be recorded and associated GHGEs estimated. In this study, the vented biogas is logged onto the server by using the SBMs, described later in the material section.

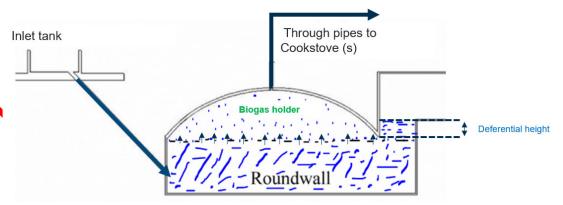


Figure 2. Biogas pressure in gasholder still under the venting threshold. Upward arrows indicate that the produced biogas under this condition (if cooking event) is collected in the biogas holder.

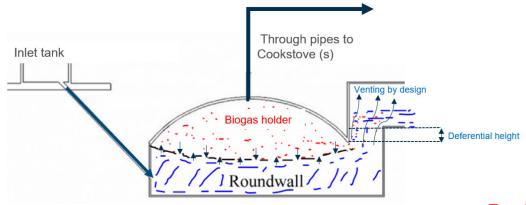


Figure 3. Biogas pressure in gasholder still above the venting threshold. The upward arrows indicate biogas being produced while the downword arrows biogas being at the same time.

Validating logged data. APGs are used as conventional measurement tools for SBP of biogas available in the biogas holder. However, APGs cannot record volumetric biogas unlisation unless when calculated from the recorded SBP and are not convenient to record instant changes in SBP. As such, SBMs are used as alternative and flexible biogas measurement tools for remote data logging, visualisation, and analysis of HH biogas unlisation for a specific HH, and in a specific time frame. To verify the reliability of results from data collected with SBMs, data validation is first done by the use of APGs. The SBP samples are recorded by the use of APGs during field visits. The SBP is sampled before and after short cooking sessions at respective technology users HHs. The sampled SBPs are used to calculate the biogas consumption by using Boyle's law, presented in Equation (1) [29], and barometric formula in Equation (2). The calculated volume of consumed biogas using APGs is compared with biogas consumption recorded with SBMs for validation. To minimise the potential effect of the produced biogas during these cooking sessions,  $p_1$  and  $p_2$  are recorded from very short cooking sessions. These sampled cooking sessions are made very short so that biogas being continuously produced from AD during the sampled cooking are assumed to be negligible.

$$V_{cons}(m^3) = \frac{(p_1 + p_2) \times V_{hol}}{p_{olim}} \tag{1}$$

$$p_{\text{otm}} = p_0 \times e^{\left(\frac{-Mgh}{RT}\right)} \tag{2}$$

 $V_{cons}$  ( $m^3$ ) is the volume of biogas consumed during the sampled cooking sessions.  $p_1$  and  $p_2$  are SBPs recorded at the start and end of a specific short cooking session respectively,  $V_{hol}$  is the volume of the biogas holder (2  $m^3$ , in this case).  $p_{alt}$  (kPa) is the local atmospheric pressure at the altitude of a specific HH.  $p_0$  is the standard atmospheric pressure (101.325 kPa), M is the molar mass of air (0.029 kg/mol), g is the acceleration due to gravity (9.81  $m/s^2$ ), g (m) is the altitude at which the biodigester is installed, g is the universal gas constant [8.314  $J/(mol\cdot K)$ ], g (K) is average temperature (temperature+273.15).

Estimating greenhouse gas emissions. After validating that the volume of biogas consumed (m³) recorded from SBMs are almost equal (with negligible differences) to the calculated values from recorded data using APGs, the biogas consumption and venting are monitored and recorded with SBMs. Using the recorded data of biogas vented over a specific period, GHGEs are estimated. Considering average local temperature over the data collection period, and the local altitude, ideal gas law is used to determine respective gas densities of CH<sub>4</sub>( $\rho_{CH4}$ ) and CO<sub>2</sub>( $\rho_{CO2}$ ) using Equation (2) and Equation (3)

$$\rho = \frac{p_{alt}}{RT} \quad , \tag{3}$$

where  $R_{CH4}$ = 518.3 J/(kg·K), and  $R_{CO2}$ =188.9 J/(kg·K) are ideal gas constant for CH<sub>4</sub> and CO<sub>2</sub> respective. A CH<sub>4</sub> GWP of 28, and CH<sub>4</sub>:CO<sub>2</sub> ratios ( $k_{CH4}$ : $k_{CO2}$ ) reported empirical literature are used. Using equations (4)–(8) and the recorded data on biogas venting (m<sup>3</sup>), the GHGEs associated with venting phenomenon over the study period are estimated. The values m, k, v,  $\rho$ , and  $E_{tot}$ , represent the masses and percentages of CH<sub>4</sub> and CO<sub>2</sub> in the produced biogas, volume, density, and total emissions, respectively.

$$E_{tot}(kgCO_{2e}) = E_{CH_A}(kgCO_{2e}) + E_{CO_2}(kg)$$
, (4)

where  $E_{tot}(kgCO_{2e})$  is the total emission in kilograms of  $CO_2$  equivalence,  $E_{CN_4}(kgCO_{2e})$  is the methane-related emission in kilograms of  $CO_2$  equivalence, and  $E_{CO}(kg)$  is the carbon dioxide-related emission. The methane emissions are obtained as equation (3)

$$E_{CH_4}(kgCO_{2e}) = m_{CH_4}(kg) \times GWP_{CH_4}$$
, (5)

where  $m_{CH_4}(kg)$  is the methane mass (kg) and  $GWP_{CH_4}$  is the global warming potential of methane. The methane mass is calculated as in equation (c).

$$m_{CH_4}(\text{kg}) = v_{biogas}(\text{m}^3) \times k_{CH_4} \times \rho_{CH_4}(\text{kg. m}^3), \qquad (6)$$

where  $v_{biogas}$  is the biogas volume in  $m^3$ ,  $k_{CH_4}$  is the methane fraction in the produced biogas and  $\rho_{CH_4}$  is the methane density. Similarly, the CO<sub>2</sub> emissions are obtained as in equation (7)

$$E_{CO_2}(kg) = n_{CO_2}(kg) \times 1$$
 , (7)

where the CO<sub>2</sub> mass (kg) is calculated as in equation (8).

$$m_{CO_2}(kg) = v_{biogas}(m^3) \times k_{CO_2} \times \rho_{CO_2}(kg.m^{-3}).$$
 (8)

<u>Establishing earses for venting</u>. Venting is the result of underutilisation of the produced biogas. Thus, the causes for underutilisation, and hence venting are analysed through a close observation of HH's cooking practices, usage patterns, interactions, and unstructured interviews during field visits.

# **Materials**

Research materials and tools used in this study are: SBMs for remote monitoring of biogas consumption and venting, a web application (WA) enhanced by machine learning algorithms (MLAs) used to remotely visualise and record biogas consumption and venting patterns, analogue pressure gauges (APGs) for validating the remotely logged data, hard notebook and log sheets for research notes during research field visits.

<u>Smart biogas metres</u>. SBMs were configured for remote data acquisition, logging, generating patterns using a WA, visualisation and recording of the biogas utilised and vented

(m³) in a specific period. The deployed SBMs rely on three sensors of two types; one measures SBP in the gas holder, while the other two measure the differential biogas pressure (DBP) to determine the biogas flow (m³/h) over a specific time (h). The SBMs used in this study are certified under IEC 61326-1:2020 [22]. The use of these SBMs for a different objective and purpose is reported by Robinson et al. [23] and Chaney et al. [24]. Sensors of the selected SBMs for this study had a maximum flow rate of 2.5 m³/h and the SBP of 10 kPa. The supplier of the SBMs had different packages but based on the determined maximum threshold pressure for venting (8kPa), as explained in subsequent sections, a safety margin of +25% (+2kPa) was allowed. Thus, SBMs with a 10kPa sensor rating was used. Based on the local experience, it was highly unlikely that more than 2.5 m³ could be consumed in an hour for a HH usage, considering that the total volume of the biogas holder was 2m³ for 8m³ biodigesters installed at respective HHs. Hence, SBMs with sensors of 2.5 m³/h flow rate was used. The used SBMs can sample data every 5 milliseconds and have the capacity to cache data for up to 24 hours, in case of data connection disruptions [23].

Web application. The sampled data are averaged every minute, stored in the cache memory, and sent to the WA every hour [23]. The WA provides a summary of biogas consumption, flow rate, static pressure over a selected time interval by using machine learning algorithms (MLA) and logged data [23]. The MLA also considers specifications of the HPI biogas plant which are specified during system configuration, e.g. the biodigester type, total volume (m³) of biodigester and volume of the gas holder (m³). The MLA detect the instantaneous gradients of the SBP in the biogas holder [24], and the WA is used to remotely monitor and analyse data on biogas utilisation and venting over a selected period.

Analogue pressure gauge. To validate data recorded by the SBMs, Analogue Pressure gauges (APGs) were installed adjacent to the SBMs. The deployed APGs can display the SBP in kPa. Based on designed venting threshold SBP of 8 kPa, APGs with a maximum SBP of 16kPa were used.

Hard notebook and log sheets. The notebook was a handy research material to record observations and responses from participating HHs members based on observed phenomenon. The objective was to record series of observations and establish the underlying causes for the observed phenomena in addition to the hard notebook, two log sheets were used. One was used during field visits for data validation, and another was kept at respective HHs to record specific SBP whenever the user was called to do so based on remotely observed pattern.

## Applying methods and materials to the case

Research methods presented earlier were customised to Rwandan HHs as a case for the study because Rwanda is one of SSA countries with a national domestic biogas programme (NDBR) [35], and its small geographical area allowed for reaching research sites flexibly. A prior literature review and interactions with biogas project officers had shown that HH biogas plants deployed in Rwanda were of three types of technologies: fixed dome, flex bags, and floating drum, although the latter is not common [26].

Because existing HH biogas plants in Rwanda, installed in the framework of NDBP were not customised to accommodating sensor-based data collection systems, new installation had to be done at selected sites. Installation of new HH plants was necessary because; (a) existing HH biodigesters installed under NDBP had technical and operation issues and had affected Rwanda's NDBP, (b) distinguishing venting from leakage required high standards of supervised installations, maintenance, and contracts obligating frequent leakage tests and reporting, (c) pipe diameters had to follow the recommended specifications from the SBMs manufacturer. Based on the forementioned gathered knowledge on the local context, this study followed a four-phases research method depicted in Figure 4.

In addition to researchers' experience and literature on Rwanda's NDBP, the local authorities recommended research sites (HHs) based on the set criteria: owning at least three cows and reliable access to piped water supply and willingness to cooperate during data collection. A review on Rwanda's biogas programme indicate that 4m³, 6m³, 8m³ and 10 m³ satisfies 42%, 62%, 82% and 104% of HH cooking energy demand in Rwandan HHs respectively [26]. Installing 10 m³ would not be economical as it would lead to the biogas underutilisation, while installing biodigesters below 8m³ would lead to insufficient gas production. Thus, 8m³ biodigesters were chosen for installation on the selected sites. Four HHs were selected for the study to ensure a daily close follow-up on the technology use and based on available budget. After selecting HHs (research sites), 8m³ HH fixed dome biodigesters were installed for research purpose.

Fixed dome technology was selected because: (a) fixed dome technology dominated existing deployments, and this would be close to simulating existing Rwanda's NDBR (b) all construction materials could be sourced locally, and (c) fixed dome technology has longer lifespan compared to flex bag (ballon-shaped polyethene biodigesters) technology also installed in Rwanda. After installation, the HH plants were fitted with SBMs to measure SBP and DBP. Conventional APGs were installed adjacently to allow for data comparison and validation during fieldwork. The research process was reviewed and approved under research permit N°:NCST/482/438/2023 issued by Rwanda's National Council for Science and Technology. The SBMs were configured by researchers while biodigesters were installed by the experienced local contractor who installed HH biodigesters through NDBP.

A differential height of 80 cm between the throat and outlet level of 8m<sup>3</sup> fixed dome technology was designed based on contractor's experience. The designed venting threshold pressure in this case was ~8kPa, a value which is dependent on the bioslurry density, differential height and acceleration due to gravity. After initial feeding, a hydraulic retention time (HRT) of 45 days was allowed based on local contractor's experience [26]. The initial feeding was properly monitored, and plants were later donated as a HH cooking lab to study the HHs' cooking practices, biogas utilisation and the venting phenomenon. After handing over the HH plants to the selected users, data was collected for a seven-months period, between 1st June –31st December 2024.

A monthly inspection was carried out by the contractor to ensure that biodigesters are leak tight. Portable electronic biogas detectors were used to detect possible biogas leakage, and monthly inspection reports were submitted to researchers. In addition to the monthly inspection report submitted by the contractor, soapy water tests to detect biogas possible leakage through pipes were conducted by researchers during field visits. Such leakage preventive mechanisms were put in place to differentiate venting from other potential biogas leakages. Further, a number of demarcations were set and SBP patterns were used to differentiate venting from other possible leakages.

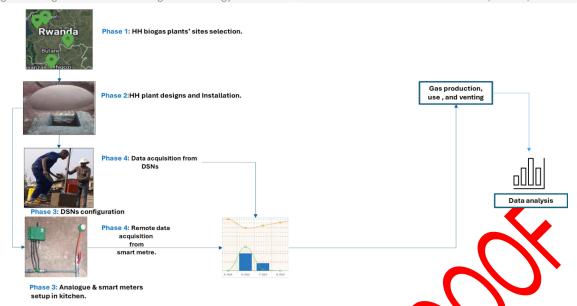


Figure 4. The four phases of the research design.

<u>Setting demarcations</u>. Venting was classified as any release of the biogas through designed outlets whenever the SBP just exceeded a set threshold value (8kPa in this case). As such, venting events could be predicted. On the contrary, any other SBP drop event that would occur due to any unpredictable, unintentional, and uncontrolled phenomena not caused by a cooking session were classified as biogas leakages.

Assumed SBP behaviour. It was presumed that whenever a venting event occurred, the SBP (absolute) remained relatively constant. This implies that that during venting events, the biogas holder has reached its maximum storage capacity, defined by the system's threshold pressure inclusive of the designated safety margin, beyond which additional biogas cannot be retained. Under this assumption, the threshold SBP (8kPa) is treated as a constant threshold pressure at which venting occurs. Under this assumption, it is recognised that biogas production varies with factors (e.g. temperature, feedstock conditions, and pH). Thus, during a venting event, it is assumed that any biogas continuously produced is vented so that the gas-holder pressure does not rise above the SBP threshold. In other words, the volume of gas being produced is balanced by the volume being vented, maintaining the pressure at the set limit. Thus, the constancy of SBP in this assumption reflects the digester's venting mechanism under leak-tight conditions, rather than an assumption of constant gas production.

Using a WA, described in the material section, three variables were remotely monitored: the average absolute SBP (kPa) in the biogas holder, the average biogas flow rate (m³/h) from the biogas holder to the biogas stove during cooking sessions, and the biogas consumption (m³) in a specific cooking duration (h). E.g, Figure 5 is used to depict a sampled event of biogas underuthisation, leading to biogas venting. It can be observed that the SBP remains relatively constant a an average SBP of about 8.5kPa, just above 8kPa (venting threshold) between 3am to 11am. On the contrary, Figure 6 indicates a recommended usage pattern, keeping SBP within a proper operation range. Selecting subsequent time slots for biogas utilisation analysis, WA enhanced by MLA helps to display biogas consumption (usage), venting, and leakage as indicated in Figure 7.

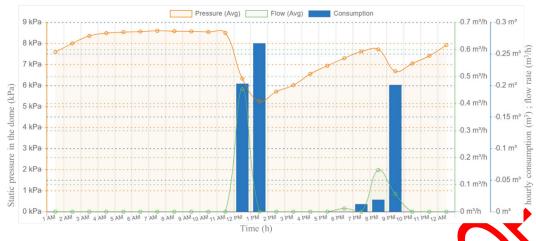


Figure 5. Biogas underutilisation pattern sampled at one of the HHs on the 13th of June 2024, between 1–12 am.



Figure 6. Recommended blogas utilisation pattern sampled at one of the HHs on the 1st of December 2024, between 1–12 am.

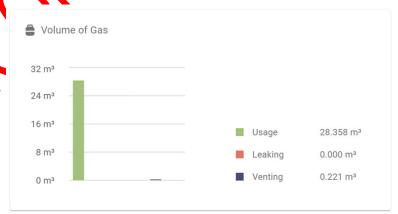


Figure 7. A sample of WA display, enhanced by MLA indicating biogas consumption (usage), venting, and leakage from the four HHs from 15th –17th July of 2024.

To this end, using equations (1)–(3), data in Table 1 was generated. Further, using the generated data in Table 1 as input to equations (4)–(8), together with recorded biogas vented (m³) from biodigesters installed at the respective participating HHs, the GHGEs were estimated.

Table 1. Local altitudes, temperatures, atmospheric pressure, CH4 and CO2 densities.

Sites	Altitude, h [m]	T [°C]	$p_{ m alt} \ [ m kPa]$	$ ho_{\mathrm{CO}_2}$ $\left[\mathrm{kg/m^3}\right]$	ρ <sub>CH4</sub> [kg/m³]
Bugesera site	1440	21	85.69	1.54	0.56
Huye site	1800	19	82.15	1.49	0.54
Musanze site	2280	18	77.56	1.41	0.51
Rubavu site	2090	18.5	79.41	1.44	0.52

### **RESULTS AND ANALYSIS**

In this section, results are presented step-by-step to answer the RQs from RQ<sub>1</sub> to RQ<sub>3</sub>. It is worth noting that no biogas leakage was detected during the data collection period. If biogas leaked, it was too negligible to be detected by the biogas leakage detectors of by the SBMs.

Figure 8 shows monthly biogas consumption and venting from the four participating HHs. Biogas vented in a seven-months period (during data collection) was 44.5 m<sup>3</sup>, 36.4 m<sup>3</sup>, 28.3 m<sup>3</sup>, and 25.6 m<sup>3</sup> for the Bugesera (Eastern), Huye (Southern), Musanze (Northern) and Rubavu (western) sites, respectively. Thus, the total biogas consumed by the participating HHs in seven months was 2,172m<sup>3</sup>, while 135 m<sup>3</sup> was lost through venting. As such, results showed that the ratio of total biogas consumption to venting was 16:1. Using recorded volume of biogas vented, equations (1–8), ratios of CH<sub>4</sub> and CO<sub>2</sub> in biogas produced from anaerobic digestion [3], and assumptions stated in methods section, the average GHGEs associated with biogas venting ranged between 33–56 kgCO<sub>2,e</sub> month<sup>-1</sup> HH<sup>-1</sup> as shown in Figure 9.

Although different HHs showed different utilisation patterns, results showed that venting levels were generally higher in the months of June, November and December compared to other months. An overall decrease in biogas utilisation was recorded in the dry season (July to early October) because of observed intermittent biodigester underfeeding at the Musanze and Rubavu sites, leading to less biogas production. Whenever biogas was used and SBP dropped below ~1.5 kPa, the biogas flow to the stove became weak and HHs were advised to wait until biogas pressure builds up. This resulted into a noticeable decrease in biogas utilisation during dry seasons. Although biogas production typically decreased during the dry season, making venting unlikely, venting events were still recorded.

Interactions with participating household members revealed that the types of meals typically prepared during the dry season were largely incompatible with the design and functionality of locally fabricated biogas stoves. The locally cooked bread prepared from corn and cassava flour requires continuous mingling and intensive physical manipulation not supported by locally fabricated biogas stove structure. Dry beans harvested in June dominated the HH's meals in the dry seasons and required prolonged cooking which requires high heat not produced by unpurified biogas used directly from anaerobic digestion. Further, the supply of fuel wood was found to be more reliable in the dry season than in the rainy season, and HHs confirmed that they preferred to cook such staple meals with fuel wood. This contributed to a low biogas utilisation in the months of July, August, September and October.

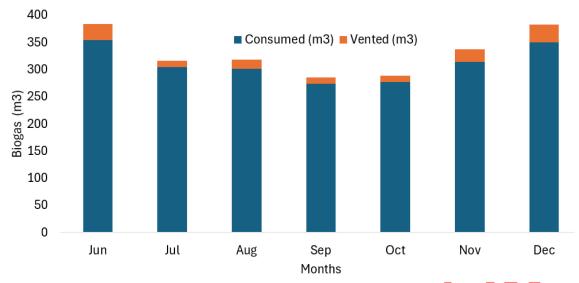


Figure 8. HH biogas monthly consumption and venting from the four HH biogas plants over a period of seven months.

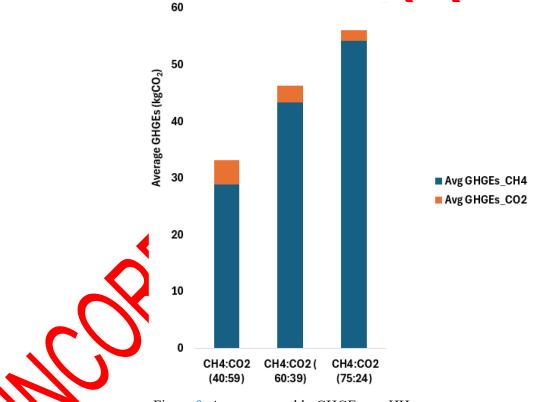


Figure 9. Average monthly GHGEs per HH.

This work answers three research questions rooted in the identified research gap, enhancing the literature on venting associated with small-scale HHBT use, specifically in SSA. The venting levels are quantified with an approach that distinguishes venting from general biogas leakage. Result showed that vented biogas led to an average monthly GHGEs of 33–56 kgCO<sub>2,e</sub> per household. Quantifying and distinguishing venting from generalised leakage can help to mitigate GHGEs associated with such a phenomenon. In this section, this study's contributions, limitations and potential future work are discussed, thereby offering a nuanced understanding of small-scale biogas utilisation and the associated GHGEs.

## Contribution to the existing literature

This study highlights that venting is a phenomenon worthy investigation while studying net-GHGEs from HH biogas use. E.g., Strubbe et al. [20] quantified net GHGEs from Rwandan households based on the assumption that 9% of biogas was lost through leakage, but such assumptions may lead to misestimations and affect voluntary carbon markets aimed to promoting HHBT use in energy-poor communities. Further, Robinson et al. [19] indicate that venting is understudied phenomenon affecting HHBT use in SSA, but results from their work are qualitative, lacking quantitative justifications. This paper adds to their work by providing quantitative findings.

The field measurements in this study confirm that the observed operating pressures are consistent with published thresholds and fall within the safe design limits for household-scale fixed-dome digesters presented in Table 2. The HH biogas systems assessed in this study were 8 m³ fixed-dome digesters, which operated close to their designed threshold of 8 kPa. Literature indicates that fixed-dome biodigesters in the 4–12 m³ range generally maintain operating pressures of 7–9 kPa, with venting or failure occurring around 8 kPa [19]. Technical manuals further specify a design maximum of approximately 9.8 kPa (100 cm H<sub>2</sub>O) across this household size range, regardless of exact volume [27].

Table 2. Safe design limits for household-scale fixed-dome digesters.

Fixed-dome digester size	Typical operating pressure	Design / relief / threshold	Discussion notes
4 m³	~ 7–8 kPa	Venting/failure at ~ 8 kPa	Robinson et al. [19] report ~ 8 kPa as a venting/failure point in household-scale fixed-dome units.
6 m <sup>3</sup>	~ 7–8 k <b>?</b> a	Design maximum ~ 9.8 kPa	Vietnam Biogas Programme [27] specifies 100 cm H <sub>2</sub> O (~ 9.8 kPa) as the safe maximum pressure for small household fixed- dome digesters.
8 m <sup>3</sup>	~ 8 kPa	Venting/failure at ~ 8 kPa	Robinson et al. [19] confirm ~ 8 kPa as the venting/failure threshold; aligns with design specifications in this study.
10 m <sup>3</sup>	~ 8–9 kPa	Design maximum ~ 9.8 kPa	Vietnam Biogas Programme [27] indicates slurry-head driven pressure with maximum ~ 100 cm H <sub>2</sub> O (~ 9.8 kPa).

The digesters in this study released an average of 33–56 kg CO<sub>2</sub>e per HH per month through venting. Although venting has long been acknowledged as a risk in small-scale digesters, quantitative household-level data expressed in CO<sub>2,e</sub> are lacking. Vu et al. [28] studied the life cycle assessment (LCA) of small-scale digesters in Vietnam. They mention biogas losses from cracks and intentional release, test sensitivity analysis and highlight venting as a factor affecting GHGEs balance but do not report household-level CO<sub>2,e</sub> values. Nou et al. 15 reports 'biogas leakage' in general terms. They report its negative effects where venting/leakage are discussed but do not provide CO<sub>2,e</sub> per HH from the venting phenomenon. Roubík et al. [29] show that of the total emissions from HHBT, 79.41% are produced during construction, 15.40% during operation, while 5.19% during demolition, but no isolated CO<sub>2.e</sub> quantification GHGEs from venting is provided. Bond and Templeton N highlight that construction quality, maintenance, and gas leakage are recurring challenges for household biogas programmes but do not report venting emissions in quantitative terms, reflecting the broader gap in standardised data on this issue. Against this backdrop, our results present field-based quantifications of household-level venting emissions expressed in CO<sub>2,2</sub> not found in existing studies, thereby filling a clear gap in the literature. These finding not only confirm that venting can contribute substantially to the climate footprint of small scale digesters but also provide data that can be directly integrated into greenhouse gas inventories and inform targeted mitigation strategies.

# On the materials used and practical limitations

Data collected by using the APG during data validation often resulted into slightly lower values compared to the logged data from the SBMs. The absolute differences are graphically presented in Figure 40, ranging between 0.01–0.04 m³. The differences may be due to the analogue readings of SRP (kPa) form the APG which are not as precise as digital data from SBMs, and/or assumed gas laws presented in methods section. The SBMs provided a convenient way for remote and timely acquisition of data on biogas utilisation and venting compared to APGs which do not provide instant data, requires physical presence of researchers and converting recorded biogas pressure from kPa to m³. Although normalised cubic meters (Nm³) are generally preferable, the off-shelf SBMs used in this study did not have the capacity to capture the continuous (e.g. temperature, atmospheric pressure) data required for accurate normalisation. Applying assumed corrections risked introducing additional uncertainties which we avoided by recording biogas volumes in m³ for consistency. While differences from Nm³ values may exist depending on temperature and pressure, these are not expected to alter the study's conclusions.

Using SBMs with Machine Learning Algorithms (MLAs) embedded in the WA provided direct readings of data required for the study. Due to the growing need of remote data acquisition in the energy sector, developing cost-effective and small-scale embedded electronic modules for HH biogas technology monitoring could enhance technology data acquisition, lead to data-driven HHBT designs and policies, and thus enhance intended benefits. Where powering such devices can be an issue due to remoteness of technology user communities, the increasing use of pico-solar modules and portable batteries can mitigate such challenges [30].

Through this study, it has been realised that contractors installing HH biogas plants in the framework of Rwanda's NDBP do not account for the effect of altitude on atmospheric pressure. This can lead to misestimations in the designing of threshold biogas pressure for venting. Rwanda's terrain is hilly and mountainous, especially in the northern and western provinces. Using the same differential height (80 cm) for 8m³ fixed dome biodigester at all sites might have marginal effects on the results.

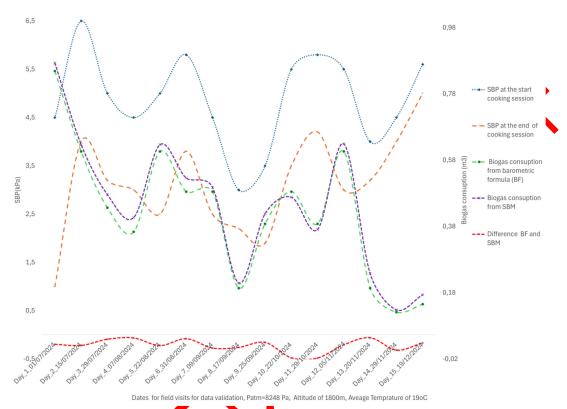


Figure 10. Data validation output from short samples of cooking sessions.

## Limitations and potential future work

This study relied on measured data and equations without modelling the anaerobic digestion (AD) process. Practically, during sampled cooking sessions for data validation, however short they may last, there is a continuous gas production through AD, and this might have marginal effects on estimations. Further studies combining anaerobic digestion modelling and the use of SBMs can add more insights to the findings of this study. Also, this work quantified the HH biogas venting levels. GHGEs associated with the venting phenomenon, and established causes of venting from HHBT by using data from 8m<sup>3</sup> fixed dome biodigester. Using different sizes and designs of biodigesters could broaden the literature on the HHBT technology use and the associated venting phenomenon. The locally fabricated and distributed biogas stoves, see Figure 11 do not follow a well standardised and regulatory framework and do not support local cooking practices and needs. Hence, technical studies focusing on how to improve and customise biogas stoves to local cooking practices, and the use of auxiliary biogas gas storage instead of venting are required to ascertain how such modifications can impact the technology use. Further still, during field work visits, it was observed that HHBT use depends on daily HH livelihoods. Thus, though this study generated insights on causes of venting, a mixed-method research approaches combining in-depth qualitative and measured data can broaden the understanding on how HH livelihoods affect the HHBT use, contributing to its sustainable use.



Figure 11. Locally fabricated and distributed biogas stove.

### **CONCLUSIONS**

This study recorded venting levels from IvH biogas plants installed in energy-poor communities. Underlying causes of HII biogas venting from HHBT use were established and GHGEs associated with such venting phenomenon calculated. Results show that vented biogas led to an average monthly GHGEs of \$3–56 kgCO<sub>2,e</sub> per household. When such results are extrapolated over a whole year this leads to average annual GHGEs of 0.4–0.7 tCO<sub>2,e</sub> per HH. Thus, HH biogas venting does not only cause loss of the biogas energy carrier but also contributes to GHGEs. Even when there is sufficient biogas for cooking, HHs opt for fuel wood to cook specific local meals which cannot be cooked by using the locally fabricated biogas stoves supplied with the HH biogas plants. Research work focusing on technical development customising the technology, especially the biogas stoves to the cooking practices of local meals, cost-effective purification methods and auxiliary biogas storage can minimise venting and enhance the envisaged technology benefits.

In addition to technical measures, demand-side practices can also help reduce venting by better matching gas availability with cooking demand. Where culturally feasible, HHs could adjust cooking times so that meal preparation overlaps more closely with peak gas production, thereby reducing pressure buildup and subsequent venting. Cooking durations may also be shortened to make biogas more suitable for foods that are typically avoided due to long simmering requirements, such as dry beans (e.g., through pre-soaking). Although some HHs may be reluctant to adopt pre-soaking dry beans because of taste preferences, such measures can be introduced as optional household-level adaptations that improve biogas utilisation and further minimise venting.

### **AUTHORSHIP CONTRIBUTION**

James Ntaganda: Literature review, conceptualisation, research methodology development, data collection, cleaning, validation, and analysis, manuscript draft, and subsequent revisions.

Basílio Zeloso Salvador Tamele: Manuscript review, discussion and editing. Erik O. Ahlgren: Supervision, conceptualisation, manuscript reviews, feedback, and editing.

### **AKNOWLEDGEMENT**

The work was done as part of and funded by the capacity building collaboration programme between University of Rwanda and Chalmers University of Technology funded by the Swedish International Development Cooperation Agency (Sida), project N°:FP1924-35. The Installation of HH biogas plants was funded by Rwanda's National Council for Science and Technology (NCST), grant N°:NCST/AIC-CAT2/002/2021.

Alphonsine Mukashyaka (a biogas engineer at EDCL, Rwanda), Oreste Niyonsaba (a social energy manager at EDCL, Rwanda), Geoffrey Gasore (a researcher in renewable energies, University of Rwanda), Jane Mukamugema (a researcher in environmental health, University of Rwanda), Evariste Twahirwa (a researcher in IoT applications, University of Rwanda), and all HH members who participated in this study are acknowledged for their discussion and/facilitation during data collection.

#### **NOMENCLATURE**

h	height	[m]
p	pressure	[kPa]
$\nu$	volume	$[\mathbf{m}^3]$
m	mass	[kg]
M	Molar mass	[kg/mol]
E	Emissions	$[kgCO_{2,e}]$

### **Greek letters**

D	density	1	[kg/m <sup>3</sup> ]

### Symbols and units

%	Percentage
$CH_4$	Methane
$CO_2$	Carbon dioxid

CO<sub>2,e</sub> Carbon dioxide equivalence

 $kgCO_{2,e}$  Carbon dioxide equivalence in kilogram  $tCO_{2,e}$  Carbon dioxide equivalence in tones

# Subscripts and superscripts

alt Altitude Consumption

tot Total

### **Abbreviations**

ABPP Africa biogas partnership programme

AD Anaerobic digestion

APGs Analogue pressure gauges

Avg Average

DBP Differential biogas pressure

DNS Data sensor network

E.g Example

GHGEs Greenhouse gas emissions

GW Global warming

GWP Global warming potential

HH Household

HHBT Household biogas technology HRT Hydraulic retention time IEA International energy agency

IEC International Electrotechnical Commission

LCA Life cycle assessment
MLA Machine learning algorithm

NCST National council for science and technology NDBP National domestic biogas programme

RQs Research questions
SBMs Smart biogas metres
SBP Static biogas pressure

SDGs Sustainable development goals

SSA Sub-Saharan Africa

STP Standard Temperature and pressure

WA Web application

### **REFERENCES**

- T. Bond and M. R. Templeton, 'History and future of domestic biogas plants in the developing world', *Energy Sustain. Dev.*, vol. 15, no. 4, pp. 347–354, 2011, doi: 10.1016/j.esd.2011.09.003.
- [2] M. Đukan and Z. Aralica, 'Analysing a Bottom-up Methodology for Developing Communal Biogas Plants in Croatia', *J. Sustain. Dev. Energy, Water Environ. Syst.*, vol. 3, no. 4, pp. 359–371, 2015, doi: https://doi.org/10.13044/j.sdewes.2015.03.0027.
- [3] A. Tolessa, 'Current Status and Future Prospects of Small-Scale Household Biodigesters in Sub-Saharan Africa, J. Energy, vol. 2024, pp. 1–19, 2024, doi: 10.1155/2024/55 5028
- [4] T. Kabera, H. Nishiniwe, I. Imanantirenganya, and M. K. Mbonyi, 'Impact and effectiveness of Ryanda's National Domestic Biogas programme', *Int. J. Environ. Stud.*, vol. 73, no. 3, pp. 402–421, 2016, doi: 10.1080/00207233.2016.1165480.
- [5] A. S. Giwa et al., 'Prospects of China's biogas: Fundamentals, challenges and considerations', *Energy Reports*, vol. 6, no. 189, pp. 2973–2987, 2020, doi: 10.1010' egy .2020.10.027.
- [6] K. Woolley, S. E. Bartington, F. D. Pope, M. J. Price, G. N. Thomas, and T. Kabera, Biomass cooking carbon monoxide levels in commercial canteens in Kigali, Rwanda', *Arch. Environ. Occup. Heal.*, vol. 76, no. 2, pp. 75–85, 2021, doi: 10.080/19338244.2020.1761279.
- [7] R. G. Hamid and R. E. Blanchard, 'An assessment of biogas as a domestic energy source in rural Kenya: Developing a sustainable business model', *Renew. Energy*, vol. 121, pp. 368–376, 2018, doi: 10.1016/j.renene.2018.01.032.
- [8] R. K. Padi, A. Chimphango, and A. P. Roskilly, 'Economic and environmental analysis of waste-based bioenergy integration into industrial cassava starch processes in Africa', *Sustain. Prod. Consum.*, vol. 31, pp. 67–81, 2022, doi: 10.1016/j.spc.2022.02.002.
- [9] J. Smith *et al.*, 'What is the potential for biogas digesters to improve soil carbon sequestration in Sub-Saharan Africa? Comparison with other uses of organic

- residues', *Biomass and Bioenergy*, vol. 70, pp. 73–86, 2014, doi: 10.1016/j.biombioe.2014.01.056.
- [10] P. Singh and A. S. Kalamdhad, 'Assessment of small-scale biogas digesters and its impact on the household cooking sector in India: Environmental-resource-economic analysis', *Energy Sustain. Dev.*, vol. 70, pp. 170–180, 2022, doi: 10.1016/j.esd.2022.07.018.
- [11] M. Ghiandelli, 'Development and implementation of small-scale biogas balloon biodigester in Bali, Indonesia', KTH, 2017. doi: diva2:1198348.
- [12] J. N. Meegoda, B. Li, K. Patel, and L. B. Wang, 'A Review of the Processes, Parameters, and Optimization of Anaerobic Digestion', *Int J Env. Res Public Heal.*, vol. 15, no. 10, pp. 1–16, 2018, doi: 10.3390/ijerph15102224.
- [13] M. Kalina, J. O. Ogwang, and E. Tilley, 'biogas revolution', *Comment Humanit. Soc. Sci. Commun.*, no. 2022, pp. 1–5, 2022, doi: 10.1057/s41599-022-013967.
- [14] Y. Chen, G. Yang, S. Sweeney, and Y. Feng, 'Household biogas use in tural China; A study of opportunities and constraints', *Renew. Sustain. Energy Rev.*, vol. 14 (2010), pp. 545–549, 2010, doi: 10.1016/j.rser.2009.07.019.
- [15] J. Hou, W. Zhang, P. Wang, Z. Dou, L. Gao, and D. Styles, 'Greenhouse gas mitigation of rural household biogas systems in China: A life cycle assessment', *Energies*, vol. 10, no. 2, pp. 1–14, 2017, doi: 10.3390/c.100.0239.
- [16] Z. Jiang, Y. Dai, and T. Du, 'Comparison of the energetic environmental, and economic performances of three household-based modern bioenergy utilization systems in China', *J. Environ. Manage.*, vol. 264, no. October 2019, p. 110481, 2020, doi: 10.1016/j.jenvman.2020.110481.
- [17] M. Jelínek, J. Mazancova, D. Van Dung, L. D. Phung, J. Banout, and H. Roubík, 'Quanti fi cation of the impact of partial replacement of traditional cooking fuels by biogas on global warming: Evidence from Vietnam', *J. Clean. Prod.*, vol. 292 (2021), 2021, doi: 10.1016/j.jclepro.2021.126607.
- [18] IEA., 'World methane emissions from energy sources, IEA estimate.' Accessed: Jan. 13, 2024. [Online]. Available: https://www.iea.org/data-and-statistics/data-tools/methane-tracker
- [19] B. L. Robinson *et al.*, 'Energy Research & Social Science Stepping on the Gas: Pathways to Reduce Venting in Household-Scale Kenyan Biogas Digesters', *Energy Res. Soc. Sci.*, vol. 121, no. September 2024, p. 103963, 2025, doi: 10.1016/j.err. 2025.103963.
- [20] L. Strubbe, A. Dierickx, B. Verbist, A. Denayer, and E. I. P. Volcke, 'Household-scale digesters in Rwanda: Performance analysis and net-greenhouse gas effect', *J. Clean. Prod.*, vol. 457, no. May, p. 142492, Jun. 2024, doi: 10.1016/j.jclepro.2024.142492.
- [21] N. Koel, 'Guideline for Biogas Generation', Ministry of Energy and Petroleum, Narobi, Kenya. Accessed: Mar. 10, 2024. [Online]. Available: https://openjicareport.jica.go.jp/pdf/12229423 03.pdf
- [22] Inclusive Energy ltd, 'Smart Biogas'. Accessed: Jan. 17, 2024. [Online]. Available: https://static1.squarespace.com/static/6380a6194d1af74b3422b87f/t/63c9415fc943bb4f9bf6763b/1674133867483/SB CE Certificate.pdf
- [23] B. L. Robinson, M. J. Clifford, and G. Selby, 'Towards fair, just and equitable energy ecosystems through smart monitoring of household-scale biogas plants in Kenya', *Energy Res. Soc. Sci.*, vol. 98, no. February, p. 103007, 2023, doi: 10.1016/j.erss.2023.103007.
- [24] J. Chaney, E. H. Owens, B. L. Robinson, and M. J. Clifford, 'Digesting data: Improving the understanding of biogas use through remote sensing', *Energy Sustain. Dev.*, vol. 86, no. February, p. 101668, 2025, doi: 10.1016/j.esd.2025.101668.
- [25] M. Landi, B. K. Sovacool, and J. Eidsness, 'Energy for Sustainable Development Cooking with gas: Policy lessons from Rwanda's National Domestic Biogas Program

- (NDBP)', *Energy Sustain. Dev.*, vol. 17, no. 4, pp. 347–356, 2013, doi: 10.1016/j.esd.2013.03.007.
- [26] Food and Agriculture Organisation, 'Biogas systems in Rwanda A critical review', Rome, Italy, ISSN 2664-6137, 2021. doi: 10.4060/cb3409en.
- [27] The Nertherlands Development Orgainisation (SNV), 'Household-scale biogas Technology (Training material for Biogas Technician)', Online Training material. Accessed: Jan. 16, 2024. [Online]. Available: https://energypedia.info/images/6/6b/EN\_Vietnam\_Training\_Manual\_Technicians\_Vietnam\_2011.pdf
- [28] T. K. V. Vu, D. Q. Vu, L. S. Jensen, S. G. Sommer, and S. Bruun, 'Life cycle assessment of biogas production in small-scale household digesters in Vietnam', *Asian-Australasian J. Anim. Sci.*, vol. 28, no. 5, pp. 716–729, 2015, doi: 10.5713/ajas.14.0683.
- [29] H. Roubík, S. Barrera, D. Van Dung, L. D. Phung, and J. Mazancová, 'Emission reduction potential of household biogas plants in developing countries: The case of central Vietnam', *J. Clean. Prod.*, vol. 270, 2020, doi: 10.1016/j.jcepro.2 \( \frac{1}{20.122257} \).
- [30] J. Ntaganda, G. Gasore, J. Mukamugema, B. Z. S. Tamele, and E. Mondlane, 'Enhancing biogas production and use by remote data acquisition and analysis-Household biogas use in Rwanda as case for the study, *2014 IEEE PES/IAS PowerAfrica*, pp. 1–7, 2024, doi: 10.1109/PowerAfrica6.667.2024.10759380.